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1 Microtomography-based Inter-Granular Network for the
2 simulation of radionuclide diffusion and sorption in a
3 granitic rock

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15 **Abstract**

Field investigation studies, conducted in the context of safety analyses of deep geological repositories for nuclear waste, have pointed out that in fractured crystalline rocks sorbing radionuclides can diffuse surprisingly long distances deep into the intact rock matrix; i.e. much longer distances than those predicted by reactive transport models based on a homogeneous description of the properties of the rock matrix. Here, we focus on cesium diffusion and use detailed micro characterisation data, based on micro computed tomography, along with a grain-scale Inter-Granular Network model, to offer a plausible explanation for the anomalously long cesium penetration profiles observed in these in-situ experiments. The sparse distribution of chemically reactive grains (i.e. grains belonging to sorbing mineral phases) is shown to have a strong control on the diffusive patterns of sorbing radionuclides. The computed penetration profiles of cesium agree well with an analytical model based on two parallel diffusive pathways. This agreement, along with visual inspection of the spatial distribution of cesium concentration, indicates that for sorbing radionuclides the medium indeed behaves as a composite system, with most of the mass being retained

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close to the injection boundary and a non-negligible part diffusing faster along preferential diffusive pathways.

16 *Keywords:* grain-scale model, diffusion experiment, anomalously long cesium
17 penetration, heterogeneity of sorption sites

18 **1. Introduction**

19 In the last two decades, the description of subsurface flow and transport
20 processes at the pore scale has received increasing attention[1, and references
21 therein]. These modelling efforts have gone hand-in-hand with the increas-
22 ing availability of laboratory instruments, such as micro computed tomography
23 (CT) scanners, which allow rock samples to be studied down to a resolution of
24 about a micron [e.g. 2, 3, 4].

25 Besides its academic value, pore scale modelling has been and is being ex-
26 tensively used by, or in the context of, the oil and gas industry, as a cheaper
27 (and, often, more reliable) alternative to laboratory experiments; e.g. to derive
28 continuum-scale properties to be used in reservoir-scale models [e.g. 5] or to
29 study physical and geochemical processes that can influence oil recovery or CO₂
30 storage in applications related to geological carbon sequestration [e.g. 6, 7, 8].

31 Recently, increasing interest has emerged in using these micro character-
32 isation and modelling techniques for the support of safety analyses of deep
33 geological repositories for nuclear waste. In this context, micro-scale studies
34 are typically applied to fractured crystalline rock formations and focused on
35 assessing the influence of the heterogeneous rock matrix on transport and geo-
36 chemical processes [9, 10]. Compared to the afore-mentioned applications in the
37 oil and gas industry, one of the main differences here is that diffusion, which is
38 retarded sometimes by sorption mechanisms, is the main (and sometimes only)
39 transport driver in the rock matrix. Moreover, fractured crystalline rocks have
40 usually a very low amount of pore space whose characteristic size is typically
41 below the resolution of micro characterisation techniques. This pore space is
42 typically found in-between grains of different mineral phases [11] and this is why

these types of micro-scale modelling approaches are denoted here as grain-scale models rather than pore-scale models.

A recent diffusion experiment (LTDE-SD experiment, [12]) carried out in the Äspö Hard Rock Laboratory (HRL) in Sweden has shown that in fractured crystalline rocks strongly sorbing radionuclides can travel surprisingly long distances driven by molecular diffusion. These anomalous penetration profiles are being assessed by an international team of experimentalists and modellers in the framework of the SKB Task Force GWFTS (Groundwater Flow and Transport of Solutes; www.skb.se/taskforce). In this study, we use grain-scale reactive transport models at different levels of detail to give a qualitative explanation to the afore-mentioned experimental results.

More specifically, we apply micro-CT analyses of a crystalline rock sample to provide a description of the inter-granular porosity which is used as topological space for numerical diffusion experiments. A detailed segmentation of the different mineral phases allows chemically reactive grains (i.e. grains where sorbing tracers could potential be sorbed on) to be identified, and sorption sites to be distributed accordingly. The numerical experiments focus on assessing whether the complex porosity network combined with the sparse distribution of sorption sites have a significant impact on the cesium penetration patterns.

2. X-ray micro-CT characterisation of the rock sample

The granodiorite sample studied here was taken from the Äspö Hard Rock Laboratory (HRL) in Sweden. The sample (LTDE-SD1) with diameter of 24 mm and length of 45 mm was drilled from an exposed fracture surface, which was the object of the LTDE-SD experiment. The rock sample includes a fracture coating with thickness of about 5 mm, an alteration rim, and an underlying less altered rock matrix (Figure 1). The fracture coating consists of calcite and quartz together with minor amounts of chalcopryrite and small crystals of barite and fluorite, and the alteration rim consists mainly of epidote and chlorite [13]. In this work we focus on the less altered rock matrix that is

72 fine-grained and according to previous studies [13] consists mainly of quartz
 73 (30–35 %), plagioclase (26–33 %), K-feldspar (26–32 %) and biotite (3–7 %).
 74 The samples studied by Widestrand et al. [13] have shown that plagioclase is
 75 partly saussuritised and sericitised, and biotite is mostly altered to chlorite. An
 76 average porosity of (0.26 ± 0.08) % has been determined for the rock matrix
 77 and it has been shown that the majority of the porosity is located at the grain
 78 boundaries around quartz and feldspar grains, and in biotite grains [13].

79 The 3D structure of the sample was determined with a SkyScan 1172 micro-
 80 CT scanner which has a conventional X-ray tube with a spot size less than
 81 $5\text{ }\mu\text{m}$ and a conical X-ray beam. The sample was scanned using a voxel size of
 82 $13.58\text{ }\mu\text{m}$, an acceleration voltage of 100 kV and a current of $80\text{ }\mu\text{A}$. Both alu-
 83 minum and copper filters were used to treat the energy spectra. During the scan
 84 2040 shadowgrams were taken with a rotation step of 0.10° . The reconstruction
 85 of the 3D image was done using a commercial software (NRecon Reconstruc-
 86 tion) with beam hardening and ring artefact removal. After 3D reconstruction,
 87 3D realization of Gaussian blur with a radius of 3 voxels was applied to reduce
 88 noise from the 3D image and to assist segmentation. Different minerals and the
 89 alteration rim were segmented from each other. First the alteration rim was
 90 segmented from the rest of the sample by detecting the interface between these
 91 two parts using the Carpet algorithm [14]. This was followed by segmentation
 92 of different minerals based on their gray value in the 3D image using histogram
 93 presentation. Threshold values for segmentation of each mineral were decided
 94 such that the thresholds were in between the peaks in the histograms. The
 95 rock matrix could be segmented into four mineral phases that include quartz
 96 and plagioclase, K-feldspar, mica minerals (biotite and chlorite) and dense ac-
 97 cessory minerals. Quartz and plagioclase could not be segmented from each
 98 other as their gray values were overlapping due to their similar X-ray attenu-
 99 ation coefficients. Furthermore, distance transform and a watershed algorithm
 100 were applied to segment the grain structure of the minerals [15]. This was done
 101 separately for each mineral phase. The original micro-CT cross section and the
 102 images obtained after the segmentation steps are shown in Figure 2.

103 The analysis described above was performed for a $1280 \times 1280 \times 1938 =$
 104 $3.18 \cdot 10^9$ voxels sized representation of the sample with a resolution of $13.58 \mu\text{m}$.
 105 The dataset was subsequently reduced by aggregating voxels up to a res-
 106 olution scale of $41.19 \mu\text{m}$ that lead to a $422 \times 422 \times 315 = 5.61 \cdot 10^7$ voxels
 107 sized representation of the sample after removal of parts including alteration
 108 rim. The resulting three-dimensional distribution of mineral grains is shown in
 109 Figure 3. The identified mineral phases in the intact rock matrix are quartz
 110 and plagioclase, K-feldspar, biotite and accessory minerals, with an abundance
 111 of, respectively, 56.1 %, 42.2 %, 1.6 % and 0.1 % of the total matrix volume.
 112 These values were found to be in fair agreement with the mineral abundances
 113 determined previously for Äspö granodiorite [13].

114 **3. Conceptual model**

115 The model mimics a typical diffusion experiment, with a cocktail of ra-
 116 dionuclides (in this set of calculations a conservative tracer and cesium) that
 117 is in contact with one face of the considered rock volume and diffuses into the
 118 rock matrix. Previous studies have shown that the properties of alteration rim
 119 and fracture coating vary highly within the experimental area of LTDE-SD in
 120 Äspö [12]. Thus our analysis focuses on the intact rock and the alteration rim
 121 was left out of this study (see Figure 3). It is worthwhile noting that in the
 122 Äspö LTDE-SD experiment, the diffusion experiment was carried out from an
 123 exposed fracture surface but also from a slim hole directly in contact with the
 124 intact rock matrix [12]. The numerical model presented in this work is quali-
 125 tatively consistent with this second experimental set-up (i.e. diffusion into the
 126 intact rock matrix).

127 Here, a constant concentration of the conservative tracer and cesium is ap-
 128 plied to the bottom boundary of the sample. Both species can penetrate into
 129 the sample driven by molecular diffusion while cesium can also sorb onto biotite
 130 surfaces.

131 3.1. Construction of an Inter-Granular Network

132 A previous study on the distribution of porosity in the LTDE-SD samples
 133 carried out using C-14-PMMA autoradiography has shown that a considerable
 134 amount of porosity lies within grain boundaries and micro fissures [13]. Hence,
 135 it is assumed here that the accessible porosity is mostly constituted by inter-
 136 granular space (i.e. space between mineral grains), whereas additional intra-
 137 granular pore space is neglected. There is evidence [4, 16, 17] that, in granitic
 138 rocks, dark minerals (e.g. biotite) contain a significant amount of intra-granular
 139 pore space. However, in the sample considered in this study there is a low
 140 amount of biotite and its mineral grains are small and sparsely distributed
 141 (Figure 2 and 3). Thus, it is considered that in this specific rock sample intra-
 142 granular space has only a minor effect on radionuclide diffusion.

143 The inter-granular space is conceptualised as a number of rectangular micro-
 144 fractures that are in contact between adjacent mineral grains. Thus, an Inter-
 145 Granular Network (IGN) is built upon a number of Inter-Granular Volumes
 146 (IGV's), which are thin rectangular cuboids of dimension $A^2 \cdot d$, being A [m]
 147 the voxel size (i.e. $41.19 \mu\text{m}$) and d [m] the inter-granular distance. A schematic
 148 representation of an IGN is shown in Figure 4. The resulting IGN for the con-
 149 sidered rock volume of LTDE-SD1 consists of 23,902,412 IGV's and 59,597,122
 150 connections, is the topological space of the reactive transport problem addressed
 151 here.

152 The distance between adjacent mineral grains (i.e. d in our model) is a
 153 highly uncertain parameter. However, a realistic assumption is that the upper
 154 threshold for d is below the resolution of the X-ray data (i.e. below $10 \mu\text{m}$)
 155 and scanning electron microscopy analyses have shown that most of the inter-
 156 granular distances are close to or below $1 \mu\text{m}$.

157 With these considerations in mind, a first model, denoted as “Base Case”
 158 (BC) model, was built using a constant inter-granular distance of $0.3 \mu\text{m}$, which
 159 resulted in a total (bulk) porosity of 0.31 %. This value is in agreement with lab-
 160 oratory measurements performed by the water immersion technique in samples
 161 drilled in the same rock volume [18].

162 To assess the influence of changes in inter-granular space, with smaller micro-
 163 fractures enhancing diffusive transport and narrowings hindering the transfer of
 164 mass, a second set of calculations was considered (“Variant Case” (VC) model).
 165 In this case the inter-granular distance was defined using a log-uniform distri-
 166 bution ($Y = \log_{10} d$) ranging between $Y = -1.5$ and $Y = 0.47$ (i.e. minimum
 167 inter-granular distance $d_{min} = 0.03 \mu\text{m}$ and maximum inter-granular distance
 168 $d_{max} = 3 \mu\text{m}$). The geometric mean of the inter-granular distance is equal to
 169 $0.3 \mu\text{m}$ (i.e. identical to the constant value used in the BC model) while the
 170 arithmetic mean is higher ($0.64 \mu\text{m}$).

171 3.2. Set-up of the reactive transport calculations

172 The resident water that fills the pore space of the sample is a typical Littorina-
 173 type water (e.g. Trinchero et al. [19] and references therein). The composi-
 174 tion of the groundwater is provided in Table 1. The same water, containing a
 175 conservative tracer in unitary concentration and cesium in trace concentration
 176 ($1 \cdot 10^{-8} \text{mol/L}$), is applied to the bottom boundary of the domain ($z=z_0$, being
 177 z_0 the origin of the z coordinate) using a Dirichlet boundary condition.

178 It is assumed that at the scale of an IGV, Fick’s law is still valid [20].
 179 Molecular diffusion in free water was set to $1 \cdot 10^{-9} \text{m}^2/\text{s}$. In the BC model
 180 local tortuosity, τ [-], was set to 0.1 resulting in a value of local diffusivity
 181 (i.e. diffusivity defined over a support volume of a single IGV) of $D_p = 1 \cdot$
 182 $10^{-10} \text{m}^2/\text{s}$. Note that the term “tortuosity” is here used in the same sense
 183 of De Marsily [21]; i.e. as the ratio between pore diffusivity and molecular
 184 diffusion in free water. This value of local tortuosity has been defined so that the
 185 resulting value of macro diffusivity (see section 4.1) is consistent with laboratory
 186 experiments carried out in a rock sample taken from the same area of the LTDE-
 187 SD experiment [18].

188 In the VC model, tortuosity is defined based on the linear expression:

$$\tau_i = \frac{1}{d_{max}} d_i \tag{1}$$

189 where subscript i indicates the i -th IGV.

Eq. (1) assumes that larger inter-granular spaces are completely open ($\tau = 1$) and that tortuosity decreases linearly with decreasing inter-granular distance. The average value of tortuosity for the VC model is $\bar{\tau} = 0.21$, which gives an average local pore diffusivity $\bar{D}_p = 2.1 \cdot 10^{-10} \text{m}^2/\text{s}$.

Cesium and the other cations sorb onto the available biotite grains (i.e. red grains in Figure 3) via cation exchange, whereas all the other mineral phases are treated as non-sorbing. The sorption model (i.e. cation exchange reactions and related selectivity coefficients - see Table 2) is taken from Kyllönen et al. [22], who assumed three different types of ion exchange sites similar to the model of Bradbury and Baeyens [23] for illite: sites on basal planes (95% abundance), interlayer sites on crystal edges (frayed-edge sites, FES) (0.02%) and a third intermediate type site (5%).

Kyllönen et al. [22] determined a mass cation exchange capacity for biotite, CEC^m , equal to $16.3 \mu\text{eq/g}$. Their experimental analysis was based on samples with a specific surface area of $0.83 \text{ m}^2/\text{g}$ (determined with BET analysis), which gives a surface specific CEC^s of $19.6 \mu\text{eq/m}^2$. Thus, for each IGV exposed to a biotite grain, a bulk site density is defined as

$$CEC_i^b[\text{eq/m}_b^3] = CEC^s/d_i \quad (2)$$

where superscript b stands for *bulk*. If none of the two neighboring grains of the IGV are biotite, then the site density is set to zero. For the sake of simplicity, in Eq.2 no distinction is made between the case where both neighboring grains are biotite and the case when only one is a chemically reactive grain.

Simulations were carried out using the reactive transport code PFLOTRAN [24, 25].

4. Results

Each reactive transport simulation run for 150 h of simulation time in the supercomputer JUQUEEN of the Jülich Supercomputing Centre [26]. For each

216 calculation, a total of 8192 processor cores were used with a wall-clock time of
 217 around 12 h. A total of about 200,000 h of supercomputing time were consumed.

218 4.1. Conservative tracer

219 The penetration of the conservative tracer is analysed by computing the
 220 average concentration at given $x - y$ cross section planes and comparing it with
 221 the analytical solution for diffusion in a plane sheet [27, 28]:

$$\frac{C(z, t)}{C_0} = 1 - \frac{4}{\pi} \sum_{n=0}^{\infty} \frac{-1^n}{2n+1} \exp\left(\frac{-D_a(2n+1)^2\pi^2 t}{4L^2}\right) \cos\frac{(2n+1)\pi(L-z)}{2L} \quad (3)$$

222 where C_0 is the boundary concentration applied at $z = 0$ and L is the total
 223 length of the domain. In the analytical model, retention processes are repre-
 224 sented using a linear isotherm sorption model. Thus, the apparent diffusivity
 225 is here defined as $D_a = D_p^*/R$, being D_p^* the macro diffusivity (i.e. diffusivity
 226 upscaled over a support volume equal to the considered rock sample) and R the
 227 retardation factor, which is defined as

$$R = 1 + \frac{K_d \rho_s}{\phi} \quad (4)$$

228 being ρ_s [g/dm³_b] and ϕ [-] the bulk rock density and porosity, respectively,
 229 and K_d [L/g] the mass distribution coefficient. For a conservative tracer, $K_d = 0$;
 230 i.e. $R = 1$.

231 The comparison between the numerical results (average concentration com-
 232 puted in 20 equally spaced $x - y$ cross sections) and the analytical solution is
 233 shown in Figure 5. The best fit with the analytical solution is obtained using a
 234 value of macro diffusivity of $5 \cdot 10^{-11}$ m²/s for the BC model and $2.5 \cdot 10^{-11}$ m²/s
 235 for the VC model. For both cases, the agreement between the numerical results
 236 and the analytical solution is very good, which indicates that, for conservative
 237 diffusive transport, the rock sample behaves as a homogeneous system. More-
 238 over, for both models the value of macro diffusivity is smaller than that of local
 239 diffusivity; more specifically, for the BC model $D_p^* = D_p/2$ while for the VC

model $D_p^* = \bar{D}_p/8.4$. This decreased macro diffusivity is the result of the intrinsic complexity of the IGN, with solute transport taking place along tortuous connections between IGV's. This effect is further enhanced in the VC model due to the presence of narrowings, which have to be by-passed by solute mass, thus increasing the overall tortuosity of the system.

4.2. Cesium

Snapshots of tracer, cesium and sorbed cesium concentration computed at 10 h and 150 h with the BC and VC models are shown in Figures 6 and 7, respectively. As already observed in the previous section, it can be noticed that, at time 150 h, the conservative tracer has traveled a longer distance in the BC model than in the VC model. By a simple visual inspection, it is evident that cesium penetrates at much slower rates than tracer as a result of sorption processes. Consistently with the underlying conceptual model, cesium is sorbed in few IGV's that are neighboring of biotite grains.

In Figure 8, a cross section located at $z = 2.59 \cdot 10^{-3}$ m is used to show snapshots of conservative tracer, aqueous cesium and sorbed cesium concentration computed with the VC model at 150 h. A smooth spatial distribution is observed for the conservative tracer. The modest concentration gradients are the result of the internal variability of diffusive pathways, which in the VC model is further enhanced by the variable distribution of inter-granular space and tortuosity. A completely different behavior is observed for cesium, which shows strong gradients between spots of high concentration and regions with very low concentration. The effect of the sparsely distributed exchange sites is evident by visually comparing the distribution of aqueous cesium and sorbed cesium concentration. Cesium is sorbed in very few exposed IGV's (i.e. the inter-granular volumes that are neighbors of biotite grains). However, these exposed IGV's behave as sinks of radionuclides and their influence on the transport of aqueous cesium extends far beyond the location of biotite grains, keeping cesium aqueous concentration at low levels also in surrounding areas. Furthermore, these cesium concentration patterns are similar to the ones observed from similar diffusion

270 experiments and analysed using autoradiographic techniques [29, 30, 12].

271 The penetration profiles of aqueous cesium obtained with the two models
272 at time 150 h are shown in Figure 9. The penetration depth is lower in the
273 VC model than in the BC model due to its lower (estimated) macro diffusivity
274 (section 4.1). These profiles are compared with the analytical solutions (Eq. 3)
275 computed with the macro diffusivity values estimated in section 4.1 and with
276 $R = 25$. The retardation factor was calibrated to match the first part of each
277 profile. An additional reactive transport calculation was carried out with a
278 homogeneous 1D system based on the bulk parameters of the BC model. In
279 this simulation, which includes the geochemical reactions described in section
280 3.2, the biotite volume fraction was set to 1.6% (i.e. same abundance as in the
281 LTDE-SD1 sample), which resulted in a total amount of sites $CEC^b = 0.77$
282 eq/m_b^3 . The comparison of both simulations points out that, for a sorbing
283 tracer, the considered rock sample is not well described by an equivalent homo-
284 geneous model. In particular, mineralogical heterogeneity leads to much longer
285 penetration depths.

286 In in-situ diffusion experiments, the rock surrounding the experimental area
287 is typically over-cored after termination of the experiment and a number of
288 small core samples are drilled from the over-cored rock volume. A post-mortem
289 analysis is then carried out by sawing the samples into slices. Each slice is then
290 analysed by means of direct activity measurements, which provide an estimation
291 of the total radionuclide mass contained in the considered slice. To mimic this
292 experimental approach, penetration profiles of total cesium mass computed at
293 150 h for the two IGN models, the analytical solutions and the homogeneous
294 simulation are shown in Figure 10. Mass is normalised by the total mass in the
295 first slice (i.e. the slice located closest to the exposed face of the rock sample).
296 As expected, given the underlying assumption of linearity, the analytical results
297 are the same already observed for aqueous concentration (Figure 9). Slight devi-
298 ations from the profiles of aqueous concentrations are observed for the numerical
299 calculations (including the homogeneous 1D simulation). These deviations are
300 the result of the non-linear sorption model, whose exchange sites might become

301 depleted, particularly close to the exposed boundary. As in the case of aqueous
 302 concentrations, none of the homogeneous models is able to capture the long
 303 penetration tails observed in the two IGN calculations.

304 The visual inspection of the spatial distribution of cesium (Figure 8) has
 305 already pointed out that the medium behaves as a composite system, with
 306 most of the mass being strongly retained close to the biotite grains and a non-
 307 negligible part of it which diffuses along preferential diffusive pathways. A
 308 similar dichotomy is observed when analysing flow through unsaturated waste
 309 rock piles, with most of the infiltrating water flowing slowly through the matrix
 310 and a small part of it being quickly channeled along macropores ([e.g. 31]).
 311 Similarly to the approach employed by Trinchero et al. [32] to simulate flow in
 312 a mining waste rock pile, here we use an alternative analytical model based on
 313 two parallel diffusive pathways:

$$C(z, t) = \alpha C_{slow}(z, t) + (1 - \alpha) C_{fast}(z, t) \quad (5)$$

314 A similar approach was also used by Cvetkovic [33] to evaluate the results
 315 of the LTDE-SD experiment.

316 In Eq.(5), both C_{slow} and C_{fast} are obtained from Eq.(3) using the values
 317 of macro diffusivity estimated for the BC and VC models but with different
 318 retardation factors. The retardation of the “slow” paths (R_{slow}) is set to 25 in
 319 both models; i.e. the same value used in the homogeneous analytical model to
 320 fit the first part of each computed profile. The retardation values of the “fast”
 321 paths (i.e. R_{fast}) and α are the calibration parameters. The best fit with the
 322 IGN calculations (Figure 11) is obtained by setting $\alpha = 0.9$, for both models,
 323 and R_{fast} to 5.8 and 4.1 for the BC and VC model, respectively. The slightly
 324 lower retardation factor of the VC model is related to the fact that the average
 325 inter-granular distance of the VC model is larger than the (constant) value
 326 used in the BC model, which results in a lower average density of exchange
 327 sites (Eq.2). The overall good agreement between the two-parallel-pathway
 328 models and the IGN results points out that the system indeed behaves as a

329 composite medium with approximately 90% of the mass being retained in or
 330 nearby strongly sorbing area, and the remaining 10% of the mass that diffuses
 331 along pathways that exhibit less retention potential.

332 It is worthwhile stressing that this composite behavior depends in turn on the
 333 ratio between the characteristic length of the problem and the average distance
 334 between chemically reactive grains. In the considered problem, the characteris-
 335 tic distance sampled by cesium is $L \sim 1 \cdot 10^{-2}$ m whereas the average distance
 336 between grains is $d_{grain} \sim 3 \cdot 10^{-3}$ m, which gives a ratio $L/d_{grain} \sim 3.3$. For
 337 larger ratios, i.e. when cesium samples a larger part of the matrix, deviations
 338 from the homogeneous behavior are expected to be less significant. A quali-
 339 tatively similar behavior is observed when interpreting drawdown data from a
 340 pumping test, with the heterogeneous aquifer acting as an equivalent homoge-
 341 neous system at late times; i.e. when the cone of depression has sampled a large
 342 portion of the aquifer [34, 35].

343 5. Discussion and conclusions

344 The SKB Task Force GWFTS is an international forum supporting the Äspö
 345 Hard Rock Laboratory activities. Within this forum, different modelling groups
 346 interact in the area of conceptual and numerical modelling of groundwater flow
 347 and solute transport in fractured rock, with special emphasis on specific in-situ
 348 experiments carried out in the HRL facility.

349 Recently, a new task (Task 9B) has been established, which aims at rein-
 350 terpreting the results of the LTDE-SD experiments. As explained in the mem-
 351 orandum of Task 9B, “[prior to the start of the Task 9B activities] *predictive*
 352 *modelling was made for the tracer penetration profiles, based on laboratory data,*
 353 *and [...] inverse modelling was made based on the obtained in-situ data. Re-*
 354 *gardless of the chosen parameters, the discrepancies between the modelled and*
 355 *observed profiles were more pronounced than the similarities”. Of special con-*
 356 *cern for Task 9B are the anomalously long penetration distances observed for*
 357 *sorbing and strongly sorbing radionuclides Nilsson et al. [12].*

358 Here, we have used a detailed micro-characterisation study of a rock sample,
 359 taken in the area of the experiment, along with grain-scale reactive transport
 360 models to offer a qualitative interpretation for these anomalously long penetra-
 361 tion profiles. The results of the calculations have pointed out that the sparse
 362 availability of exchange sites has a strong influence on the observed cesium pen-
 363 etration pattern. The profiles of cesium penetration agree well with a simplified
 364 lumped model based on two parallel diffusive pathways. This match points out
 365 that, for sorbing radionuclides, the considered rock volume behaves as a com-
 366 posite medium, with most of the mass (around 90%) being retained close to
 367 the injection boundary and a non-negligible part of the solute (around 10%)
 368 moving faster along preferential diffusive pathways. A qualitatively similar be-
 369 havior is observed in different cores drilled in the experimental area of LTDE-SD
 370 and a similar parallel pathways model was successfully used by Cvetkovic [33]
 371 to provide a quantitative explanation to these observed anomalous penetration
 372 profiles.

373 Other main conclusions of the work are:

- 374 • the penetration profiles of the conservative tracer resemble those obtained
 375 from homogeneous models. The intrinsic complexity of the IGN results in
 376 a macro diffusivity that is lower than the values set at the scale of a single
 377 IGV.
- 378 • when internal variability of inter-granular space is taken into account,
 379 macro diffusivity is further decreased due to the effect of narrowings, which
 380 have to be by-passed by diffusing solutes.
- 381 • active grains behave as sinks for aqueous radionuclides and their influence
 382 extends far beyond the location of the grains itself.

383 It is worthwhile noting that the conclusions obtained from this work do not
 384 exclude other (additive) effects that could be important over the (larger) scale
 385 of the LTDE-SD experiment. Features that might also contribute to anomalous

386 penetration profiles (also for conservative tracers) are cm-scale fractures and
387 skin effects due to local stress redistribution [36].

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Table 1: Chemical composition of the groundwater used in the reactive transport calculations.

Total concentration (mol/L)	
Na ⁺	3.3×10^{-2}
K ⁺	6.1×10^{-4}
Ca ²⁺	9.5×10^{-4}
Cl ⁻	3.1×10^{-2}
SO ₄ ²⁻	2.1×10^{-3}

Table 2: Cation exchange reactions and selectivity coefficients (Gaines-Thomas convention) [22].

Reaction	Selectivity coefficients ($\log K$)
Planar sites	
$X^- + Na^+ \leftrightarrow NaX$	0.0
$X^- + K^+ \leftrightarrow KX$	2.3
$X^- + Cs^+ \leftrightarrow CsX$	2.0
Intermediate sites	
$X_{int}^- + Na^+ \leftrightarrow NaX_{int}$	0.0
$X_{int}^- + K^+ \leftrightarrow KX_{int}$	2.3
$X_{int}^- + Cs^+ \leftrightarrow CsX_{int}$	4.5
Frayed-edge sites	
$X_{FES}^- + Na^+ \leftrightarrow NaX_{FES}$	0.0
$X_{FES}^- + K^+ \leftrightarrow KX_{FES}$	2.5
$X_{FES}^- + Cs^+ \leftrightarrow CsX_{FES}$	8.0

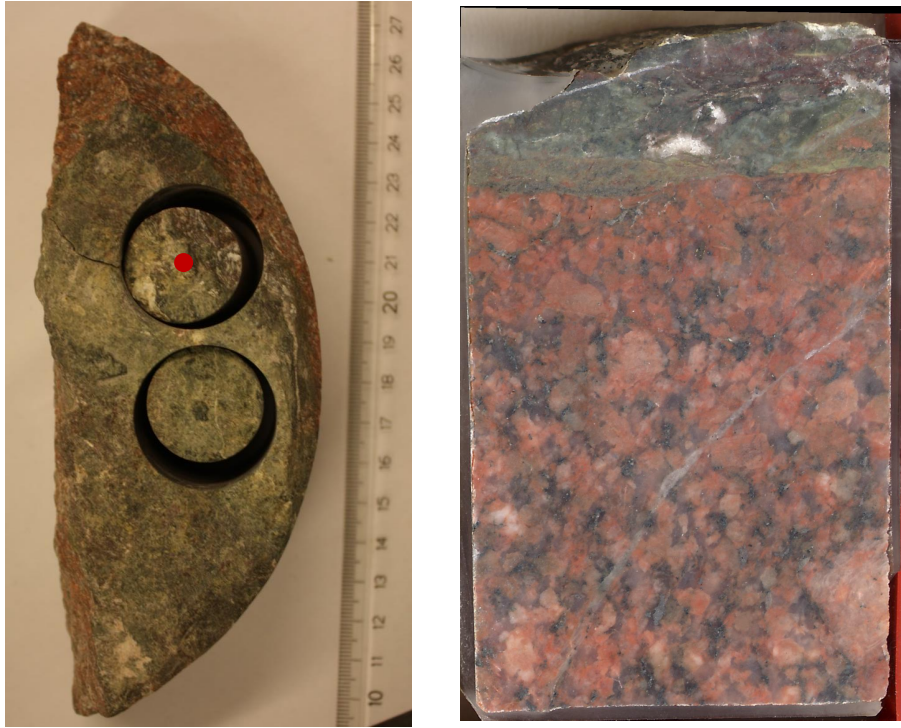


Figure 1: (left) The LTDE-SD samples from the Äspö HRL (Sweden) and (right) cross section of sample LTDE-SD1, which is the object of this study (sample LTDE-SD1 is also indicated with a red dot in the picture to the left).

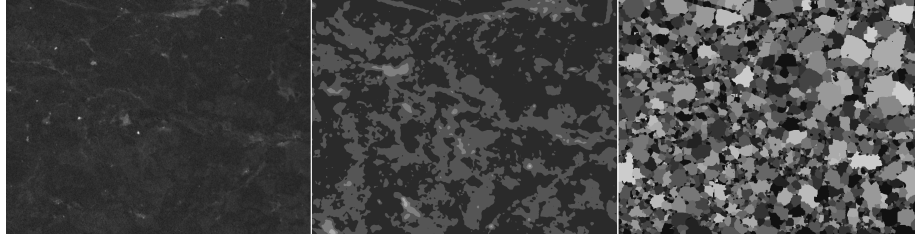


Figure 2: Cross sections of the LTDE-SD1 sample showing original micro-CT (left), map of segmented mineral phases (center) and map of segmented mineral grains (right). In the map of segmented mineral phases quartz and plagioclase (dark gray), K-feldspar (gray) and biotite (light gray) are shown.

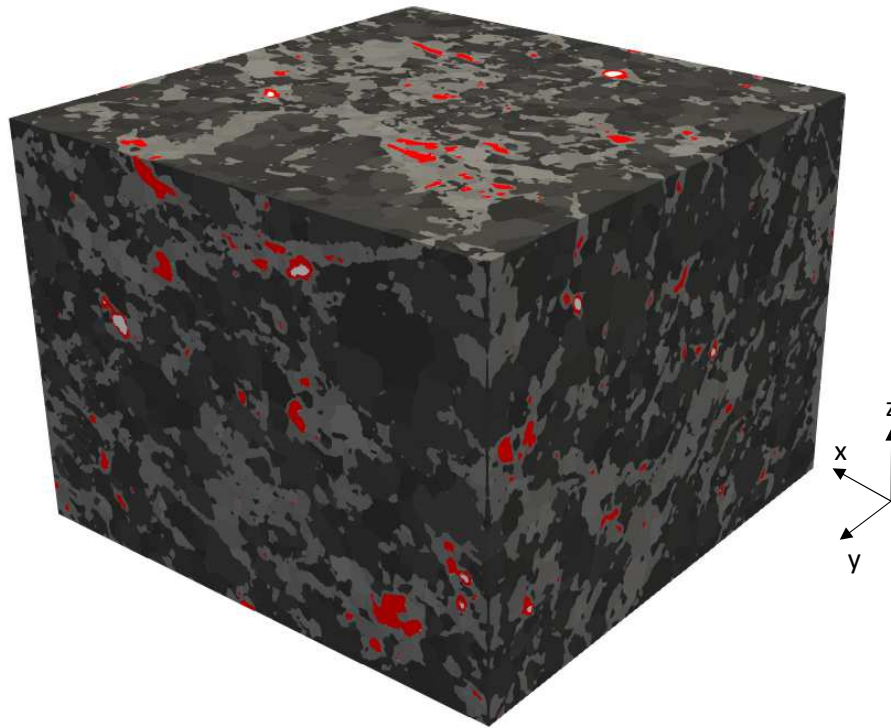


Figure 3: Three-dimensional visualisation of the LTDE-SD1 sample after mineral segmentation. Only the part of the sample considered in the calculations is shown ($1.7 \cdot 10^{-2}$ m x $1.7 \cdot 10^{-2}$ m x $1.3 \cdot 10^{-2}$ m). Biotite grains are displayed in red.

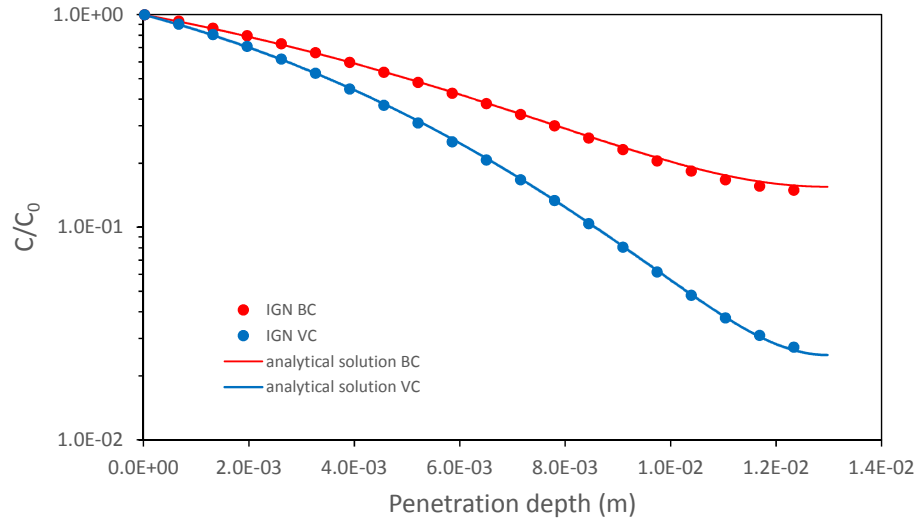


Figure 5: Penetration profiles for the conservative tracer computed at 150 h for the BC (red dots) and VC (blue dots) models. Both results can be fitted with the analytical solution for diffusion in a plane sheet (Eq.(3) and continuous lines). The best fit with the analytical solution is obtained using a value of macro diffusivity of $5 \cdot 10^{-11} \text{m}^2/\text{s}$ for the BC model and $2.5 \cdot 10^{-11} \text{m}^2/\text{s}$ for the VC model.

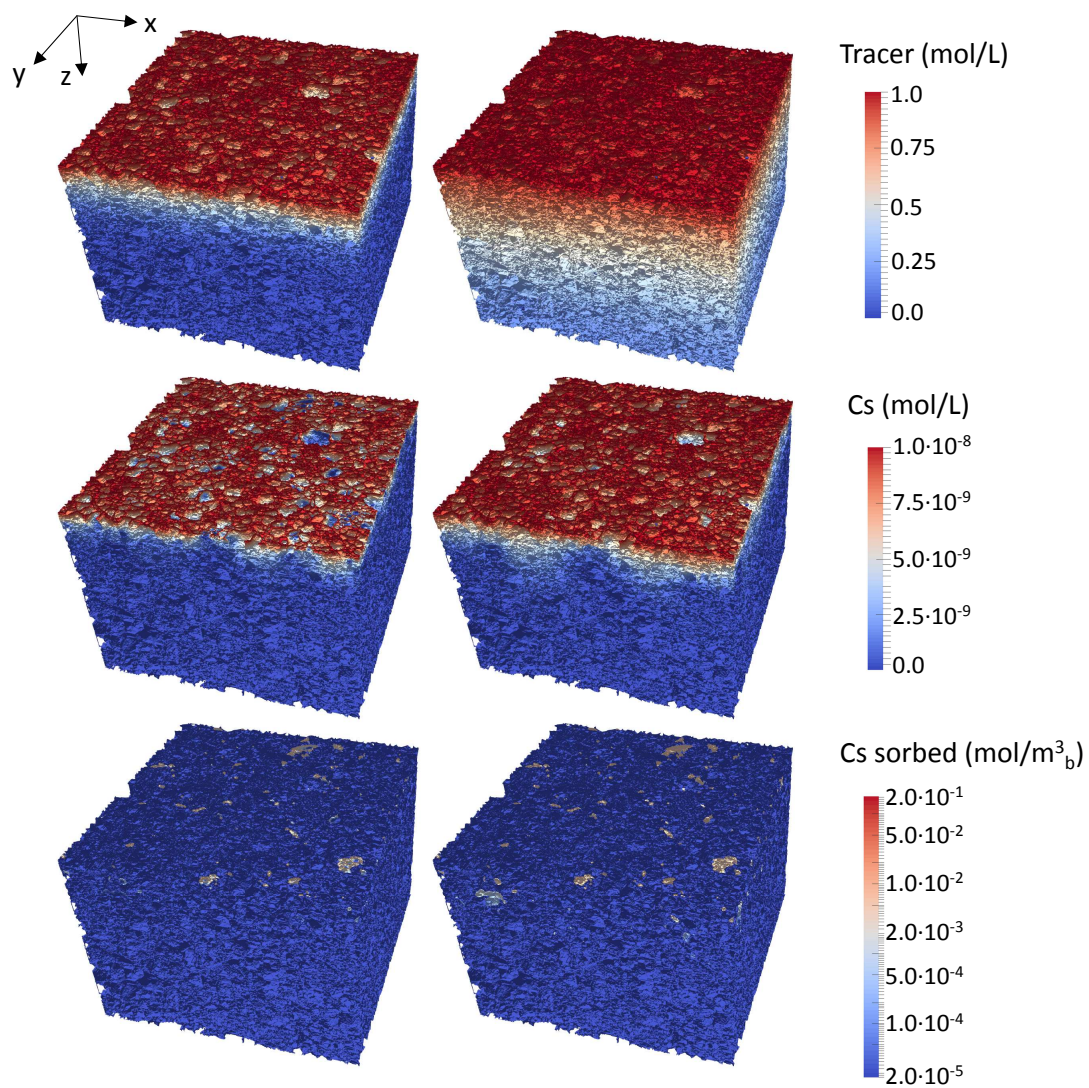


Figure 6: Snapshots of (top) conservative tracer, (middle) aqueous cesium and (bottom) cesium sorbed computed at (left) 10 h and (right) 150 h with the BC model.

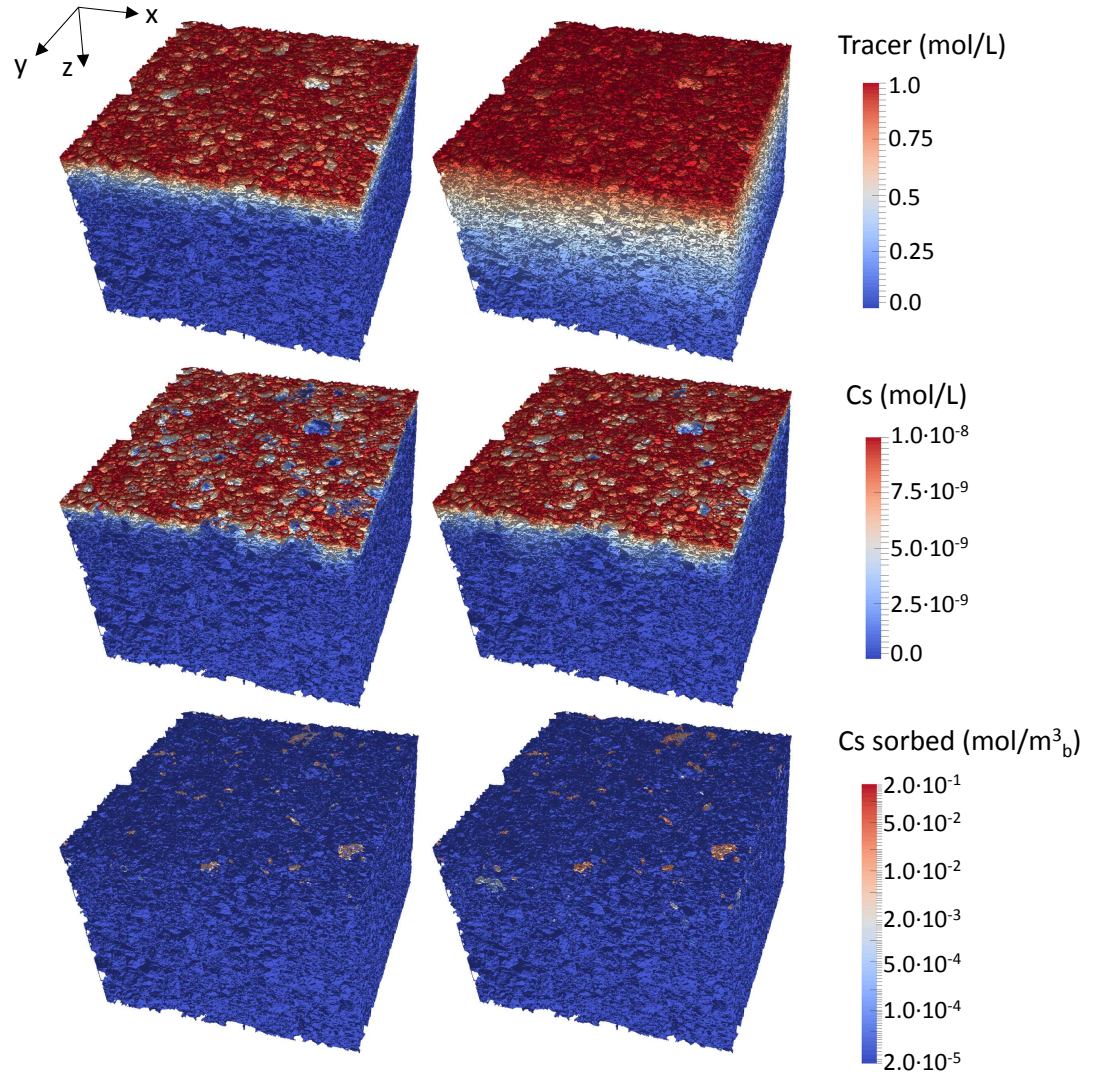


Figure 7: Snapshots of (top) conservative tracer, (middle) aqueous cesium and (bottom) cesium sorbed computed at (left) 10 h and (right) 150 h with the VC model.

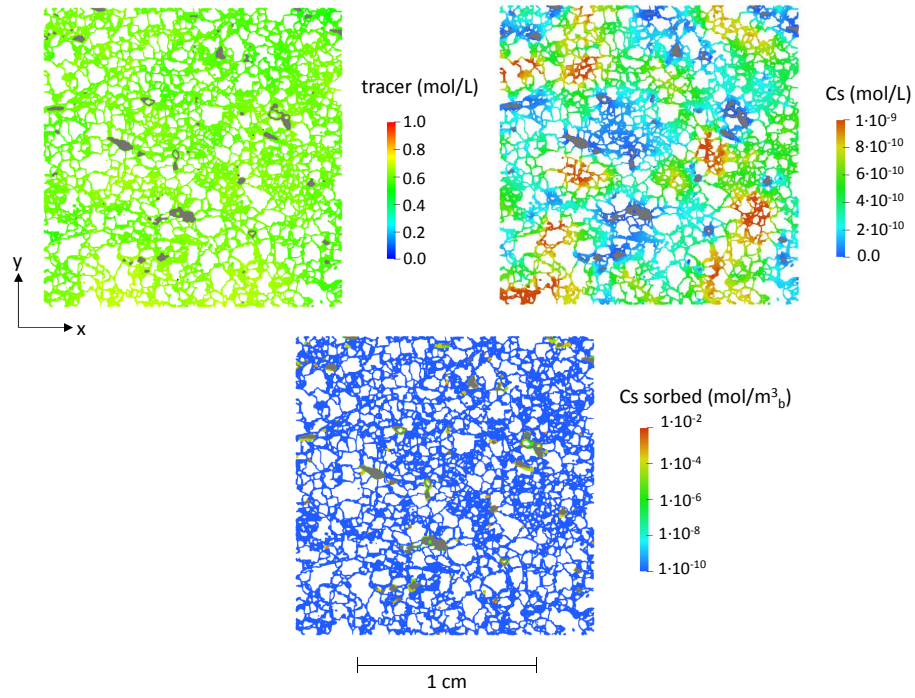


Figure 8: Distribution of (top-left) conservative tracer, (top-right) aqueous cesium and (bottom) sorbed cesium concentration computed at 150 h with the VC model. Results are shown in a cross section taken at $z = 2.59 \cdot 10^{-3}$ m. Gray shaded areas represent the biotite grains.

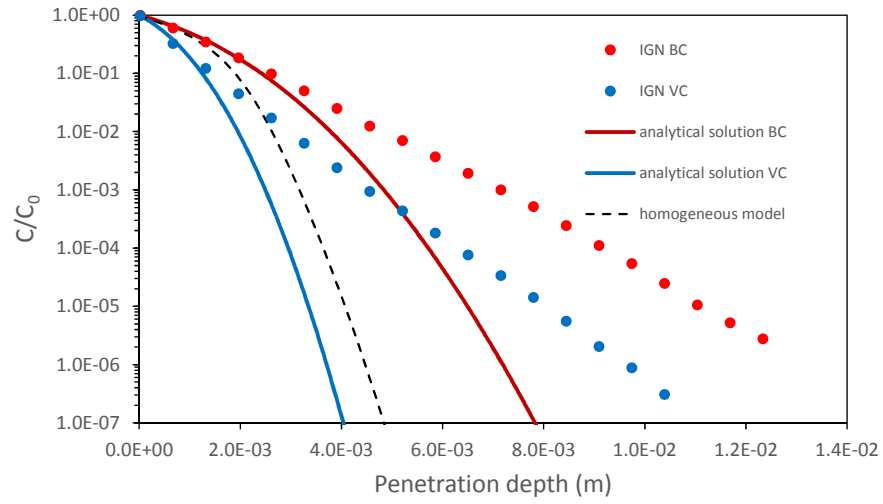


Figure 9: Penetration profiles for cesium (aqueous cesium concentration) computed at 150 h for the BC (red dots) and VC (blue dots) models. The analytical solutions used to fit the numerical results are shown with continuous lines whereas the dashed line shows the results of a numerical calculation based upon a homogeneous distribution of the available exchange sites.

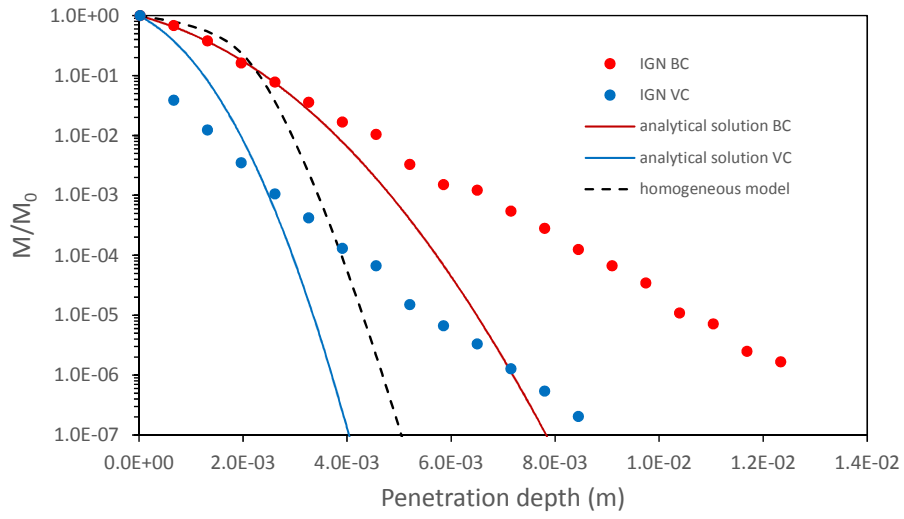


Figure 10: Total mass of cesium computed at 150h for the BC (red dots) and VC (blue dots) models. The analytical solutions used to fit the numerical results are shown with continuous lines whereas the dashed line shows the results of a numerical calculation based upon a homogeneous distribution of the available exchange sites. Mass is normalised by the total mass close to the injection boundary.

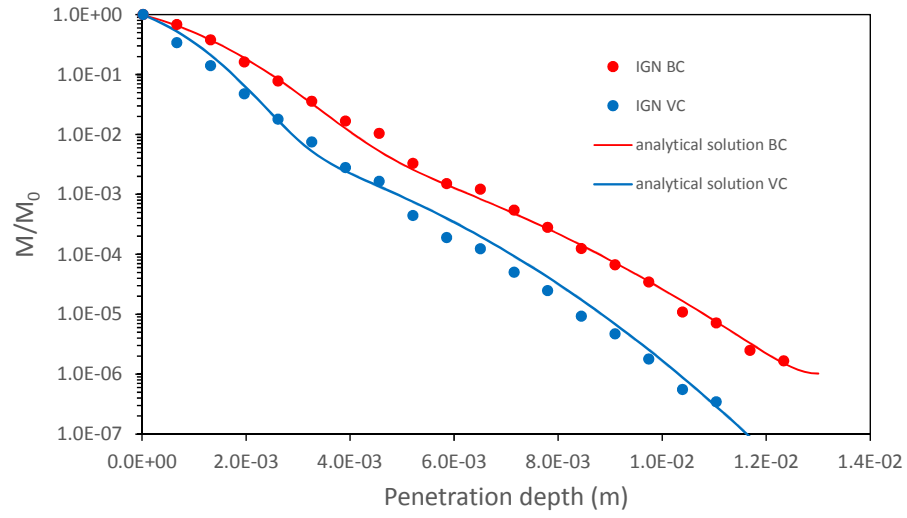


Figure 11: Total mass of cesium computed at 150h for the BC (red dots) and VC (blue dots) models. The continuous lines are computed using the analytical two-parallel-pathway model.